

# Discrete and hybrid models: Applications to concrete damage

Václav Šmilauer

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# About me

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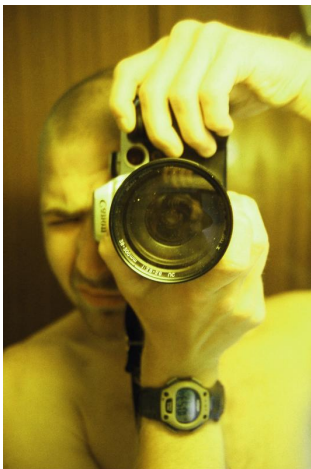
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- PhD student, financed by French ministry of research this year.
- Enrolled both in Prague (Milan Jirásek) and Grenoble (Laurent Daudeville) – “doctorat en co-tutelle”.
- Work focusing on Yade:
  - open-source platform for numerical calculations, since 2003;
  - continuing development, funded mostly by laboratory 3S-R in Grenoble.

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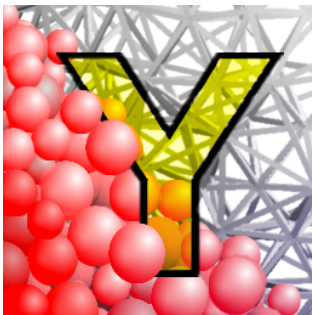
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<http://yade.wikia.com>

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# (Primarily) continuous models

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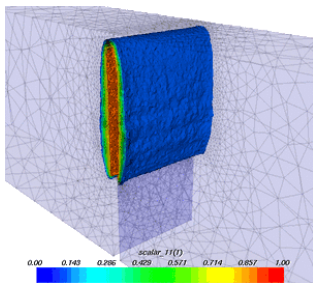
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- Problem formulated in terms of differential equations – continuum mechanics.
- Displacement function  $u$ , found by numerical solution of boundary value problem.
- Discontinuities in  $u$  are an extension of the method.
- Strain undefined at discontinuity, “awkward” (sophisticated) methods.



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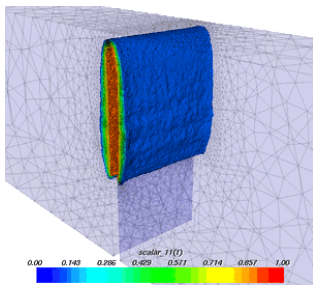
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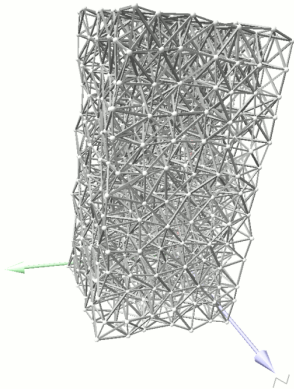
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- Local equations determine global behavior numerically – element interactions.
- No integration necessary, more computationally intensive.
- Discontinuity description trivial.
- Continuity (cohesion) by linking elements.
- Discrete element method (DEM).
- Lattice models.

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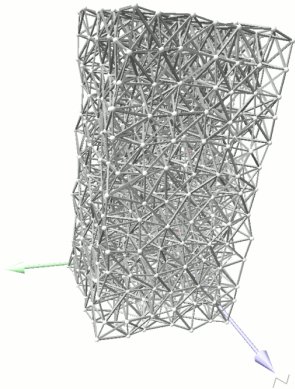
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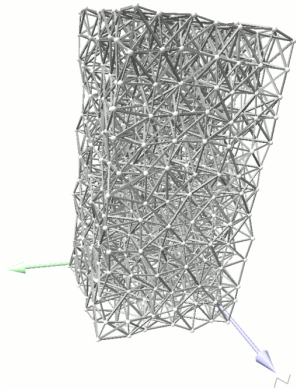
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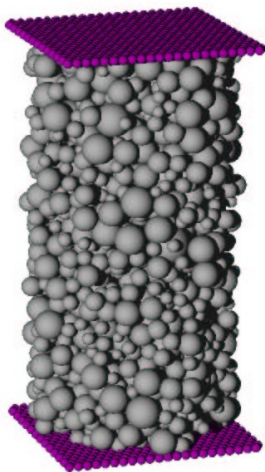
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- elements are rigid bodies, motion governed by Newton's laws
- explicit integration in time
- “smooth” (pinball) vs. “non-smooth” (overlaps) DEM
- mechanics of granular media — Cundall, 1971 (“distinct element method” in 2D, spherical elements)
- molecular dynamics of gas (1980s)

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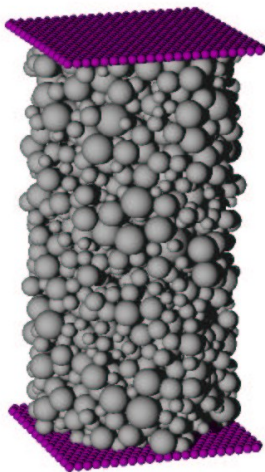
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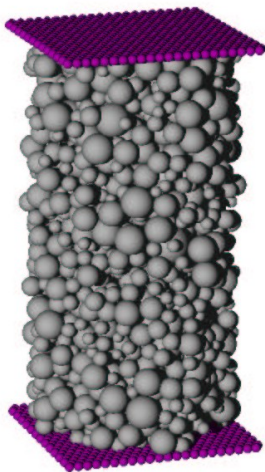
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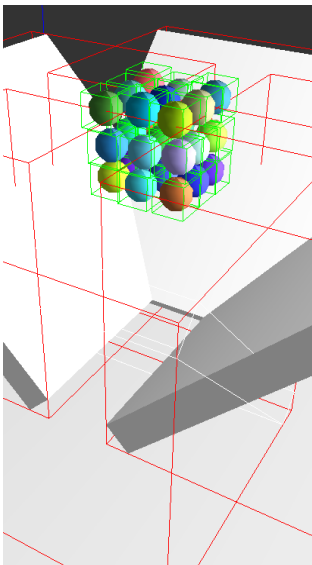
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How to calculate spheres falling  
through a funnel?

- Known element constants ( $m$ ,  $\mathbf{I}$ , ...)
- and variables at  $t = t_i$  ( $\mathbf{x}$ ,  $\mathbf{o}$ ,  $\mathbf{v}$ ,  $\omega$ , state parameters).
- Solve for variables at  $t = t_{i+1} = t_i + \Delta t$ .



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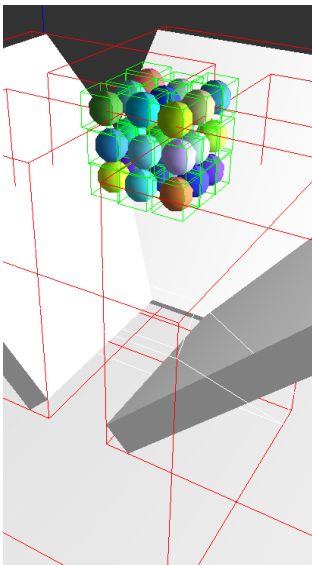
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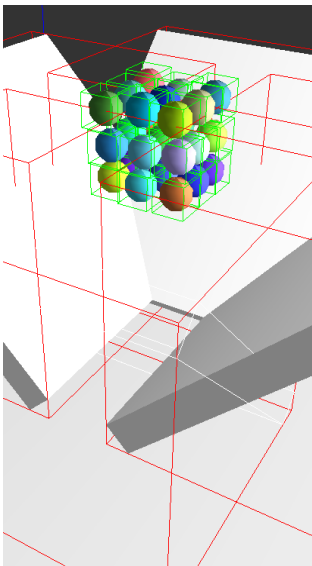
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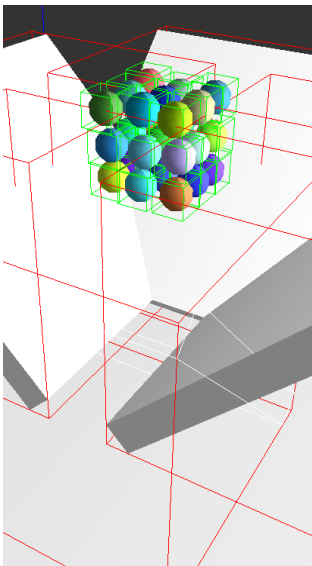
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# DEM iteration

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```
void SphericalDEMSimulator::doOneIteration()
{
    // compute dt
    if (useTimeStepper)
        dt=computeDt(spheres,contacts);
    // detect potential collision
    sap.action(spheres,contacts);
    // detect real collision
    findRealCollision(spheres,contacts);
    // compute response
    computeResponse(spheres,contacts);
    // add damping
    addDamping(spheres);
    // apply response
    applyResponse(spheres);
    // time integration
    timeIntegration(spheres);
}
```

## 1 Calculate forces:

- independent fields,
- inter-element links,
- element collisions.

## 2 Calculate acceleration from forces.

## 3 Integrate over $\Delta t$ , $t = t_i + \Delta t$ .

## 4 (Adjust $\Delta t$ .)

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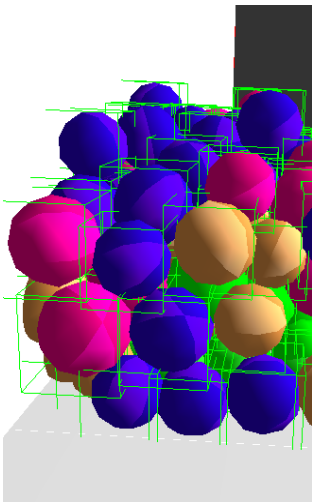
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Big research issue in applied mathematics, trivial approach is  $O(n^2)$ . Better approach:

- 1 Replace each element by its AABB (Axis-Aligned Bounding Box).
- 2 Sort  $x$ ,  $y$ ,  $z$  min-max arrays independently.
- 3 Overlaps on all coordinates are *collision candidates*.
- 4 Candidates tested geometrically for collision.

# Collision detection

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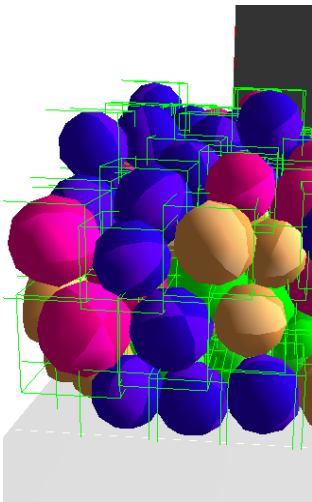
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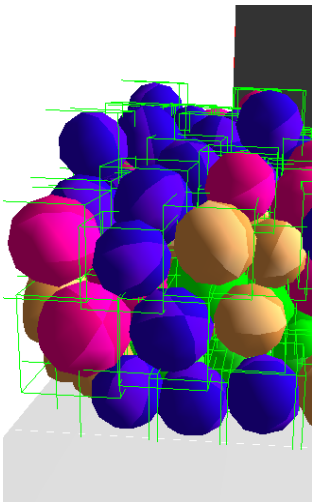
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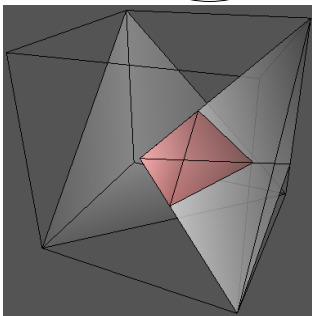
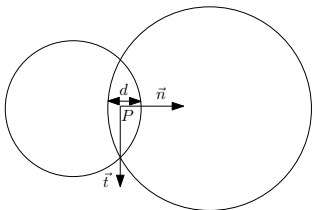
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Geometry:

- $P$ ,  $n$ ,  $t$ ,  $d$  for spheres (trivial).
- Complicated for other shapes (e.g. tetrahedra:  $C$ ,  $V$ ,  $I$ ).
- Combinations: sphere with tetrahedron, parallelepiped, ...

Forces are yet to be found.

# Collision detection

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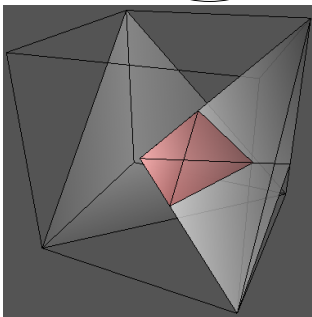
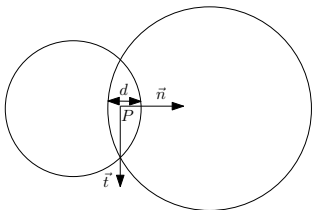
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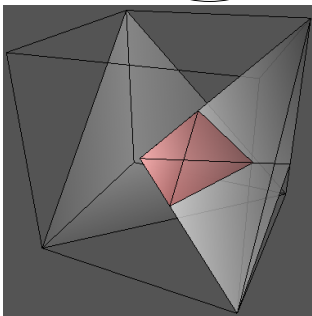
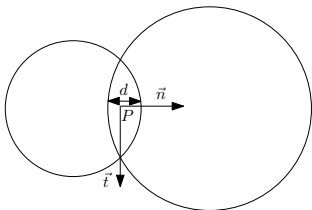
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# Physical laws

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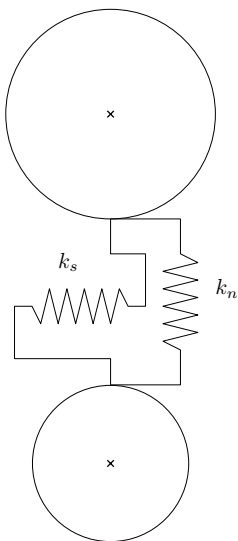
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The most simple model:

- $F_n = k_n d$ ,  $\Delta F_s = k_s \Delta u_t$  (incremental).
- Fracture with Coulomb criterion  $\max F_s = F_n \tan \phi$ .

How to determine  $k_n$ ,  $k_s$  from macroscopic characteristics?

- Simplistically for sphere  $F = Ku$ ,  $F = \sigma S = E(1 - d/2r)\pi r^2$  ( $d \ll r$ )
- Really used formulas: coefficients without physical meaning.

→ Model calibration.



# Physical laws

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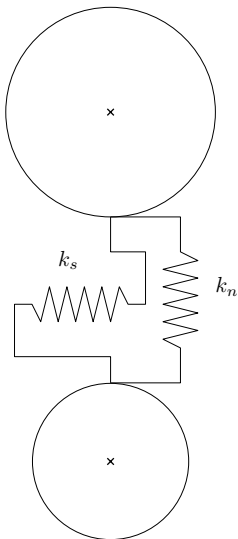
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# Mesh generation

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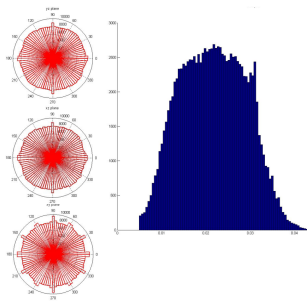
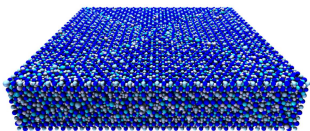
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- Requirements: isotropy, high coordination number and compacity, size distribution.
- Regular packing leads to anisotropic behavior.
- Dynamic methods: gravity, growing spheres. Slow.
- Jean-François Durier: Geometric method based on tetrahedral mesh:
  - Leverages existing FEM meshers — arbitrary shapes.
  - Very fast with excellent parameters.

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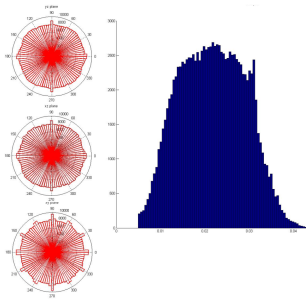
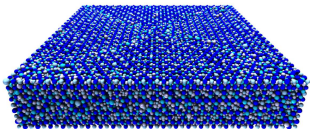
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- Requirements: isotropy, high coordination number and compacity, size distribution.
- Regular packing leads to anisotropic behavior.
- Dynamic methods: gravity, growing spheres. Slow.
- Jean-François Durier: Geometric method based on tetrahedral mesh:
  - Leverages existing FEM meshers — arbitrary shapes.
  - Very fast with excellent parameters.

# DEM concrete fracture (Hentz)

Discrete and hybrid models:  
Applications to concrete damage

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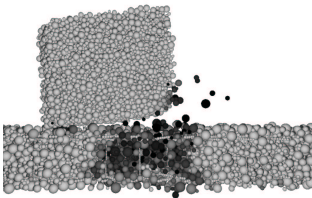
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*Modélisation d'une Structure en Béton Armé Soumise à un Choc par la Méthode des Éléments Discrets* (PhD thesis of Sebastian Hentz, 2003)

- Dropping reinforced concrete cube on reinforced concrete slab.
- Concrete elements not “physical” (matrix, inclusions).
- Reinforcement modelled by special elements (including plastification).
- Parameters calibrated on basic setups, not *ex post* — predictive value.

# DEM concrete fracture, results

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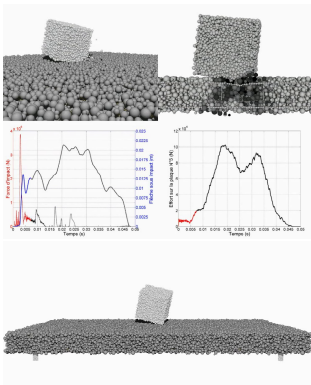
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- 80+110 thousand elements (reinforcement + concrete)
- Comparison with instrumented experiment at different limit states.
- + Good results (e.g. displacements  $\pm 10\%$ ).
- Long calculation

# Lattice overview

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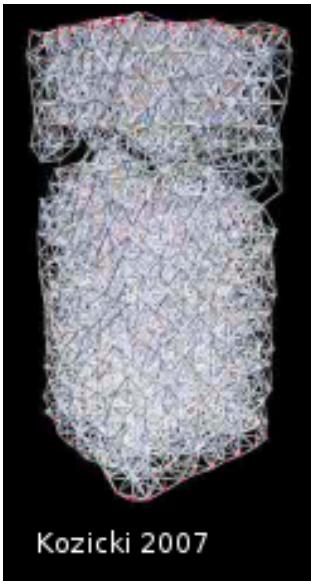
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- Replaces continuum by arrangement of 1D elements (trusses, rods, beams).
- Nodes may carry inertia mass (dynamic) or not.
- Irregular meshes, less sensitive to degenerate geometry.
- Voronoï tessellation / Delaunay triangulation.

# Lattice beam model (Cusatis & co.)

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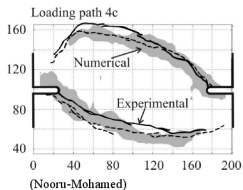
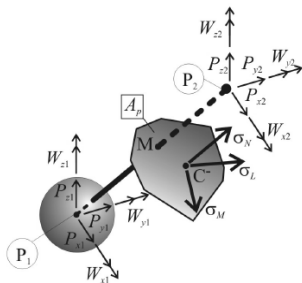
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- Meso-scale lattice *beam* model (matrix, inclusions).
- Constitutive law with damage, fracture, plasticity.
- Elaborate beam properties based on geometry of the respective Voronoi cell.
- Good match in tensile as well as compressive (usual weak point of lattices) loading.

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## FEM

- + Efficient and easy for undamaged continuum.
- Difficult discontinuity description.
- Undamaged zone.

## Lattice

- + No collision detection necessary.
- No volumetric information.
- Fragmenting zone interior.

## DEM

- + Compressive links created during simulation.
- Collisions: computationally expensive.
- Highly fragmented, collapsing zones.
- Colliding boundaries or detached zones.



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# FEM inside DEM

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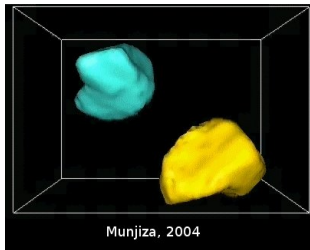
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- Particles in DEM are themselves FEM domains.
- Interest: reduces computational expenses wrt pure DEM for unfractured parts.
- Allows for dynamical states — in pure FEM, leads to statically under-determined states.
- More difficult collision detection (mesh — mesh).
- For non-predetermined fracture, FEM→DEM transition (via crack modeling and tracing) must be provided.

# FEM next to DEM

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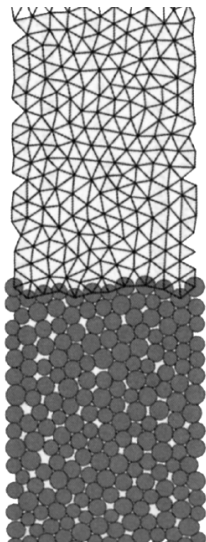
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Cundall & al. 2003



- Part of domain expected to break is DEM, the rest is FEM.
- Reduces computation wrt pure DEM.
- Must know fracturing (DEM) domain beforehand.
- Parameters must be tuned to have similar elastic behavior in both domains.
- The domain interface reflects waves (remedy: overlap zone — E. Frangin).



# DEM with lattice

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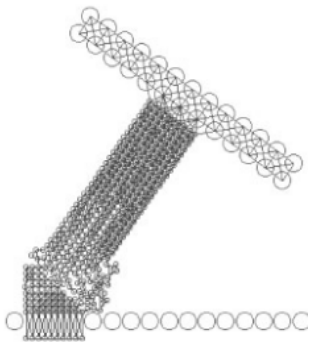
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Sun & al, 2003

- Nodes are also DEM elements.
- Or: boundary nodes are DEM (collision), insert equivalent DEM element as needed.
- Preserves volume when fractured; pure lattice collapses.

# References

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